







# Proposal for the optimal management of a DC microgrid

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# I. Introduction

















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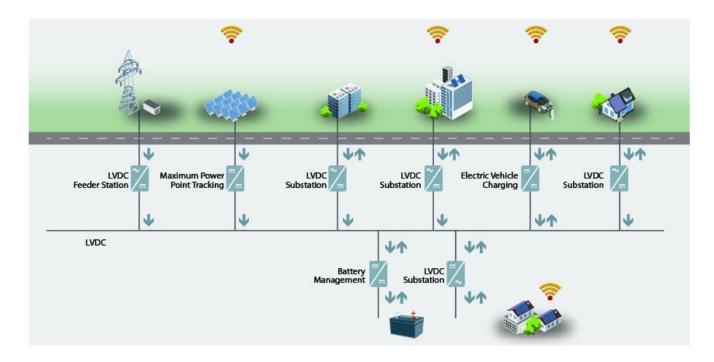
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- Particular features of local geography make difficult to provide electricity to communities at certain rural zones.
- In isolated (i.e. non interconnected) areas, DC microgrids can be used to attend electric power demand.







https://www.danfoss.com/en/about-danfoss/articles/dds/new-power-network/





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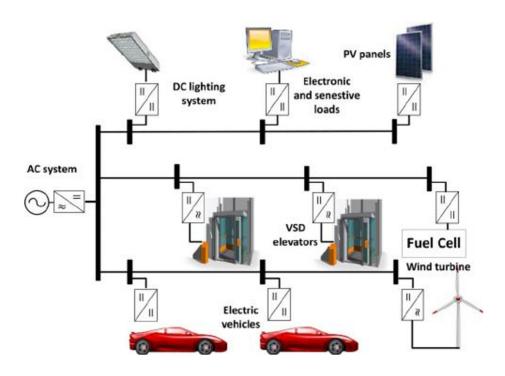
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- DC generators are simple to control as they avoid parameters like frequency and phase.
- The reduced complexity of DC microgrids is reflected in a further reduction of costs.
- The development of low-cost, microgeneration systems including renewable sources, becomes an interesting topic for R&D projects supporting economical and social development at isolated zones.







Hamad, Amr & Farag, Hany & El-Saadany, Ehab. (2015). A Novel Multiagent Control Scheme for Voltage Regulation in DC Distribution Systems. IEEE Transactions on Sustainable Energy. 6. 1-12. 10.1109/TSTE.2015.2391114.





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- The situation becomes more critical when the microgrid is isolated.
- Conventional economic dispatch policies are based on fuel prices and consider renewable energies as free resources.













### **Problem statement**



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### **II. Hierarchical control**





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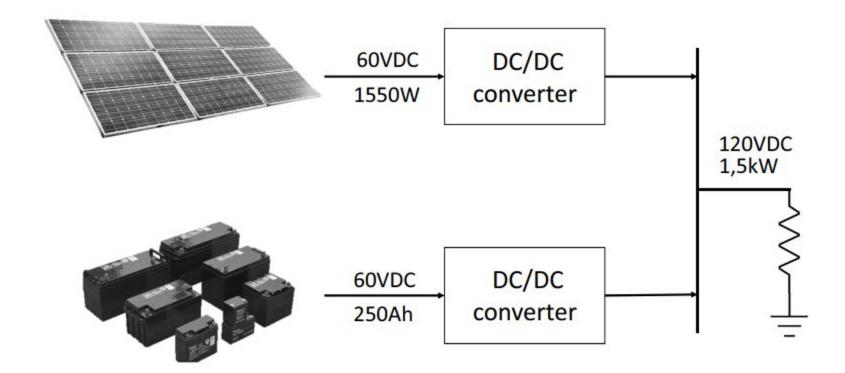
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- In the case of DC microgrids the *droop parameter* is a resistance relating variations in voltage and power.
- For illustration of the technique, let us consider an isolated microgrid composed of a PV array in parallel with a battery bank, feeding a pure resistive load.











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- Equivalent circuits for generators and disturbances were implemented in PSIM.



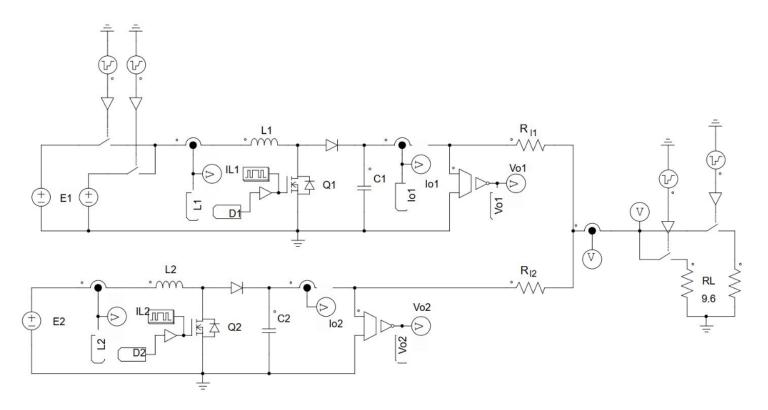
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- Equivalent circuits for generators and disturbances were implemented in PSIM.
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- Impedance of transmission lines representing physical connections between output ports of each generator and the load bus, were modelled as resistors.











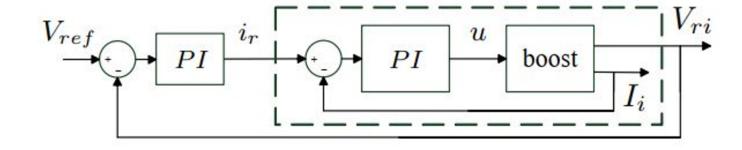
Parameter	Description	Value
$E_1$	Supply voltage at PV source	60 VDC
$E_2$	Supply voltage at batteries	60 VDC
$L_1 = L_2$	Inductance of boost converter	5.6 mH
$C_1 = C_2$	Capacitor of boost converter	100 μF
$Q_1 = Q_2$	IGBT of boost converter	ideal
$D_1 = D_2$	Nominal duty cycle of converter	0.5
$R_{l1}$	Coupling resistance converter 1	0.032 Ω
$R_{l2}$	Coupling resistance converter 2	0.016 Ω
f	Nominal PWM frequency	20 kHz
V	Nominal voltage at DC bus	120 VDC
$R_L$	Nominal system load	9.6 Ω



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$$R_{di} \leq \frac{\Delta V \times V_{\sigma}}{P_{\sigma_i}},$$

being  $\Delta V$  the maximum deviation allowed for the DC bus voltage,  $P_{\sigma_i} = I_{\sigma_i} \times V_{\sigma}$  the maximum power delivered to the load by the i-th generator and  $V_{\sigma}$  its minimum voltage.

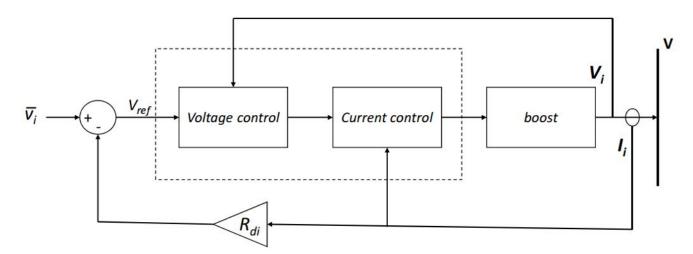




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- The secondary level defines, by mean of droop resistances, the proportion of power shared among generators.

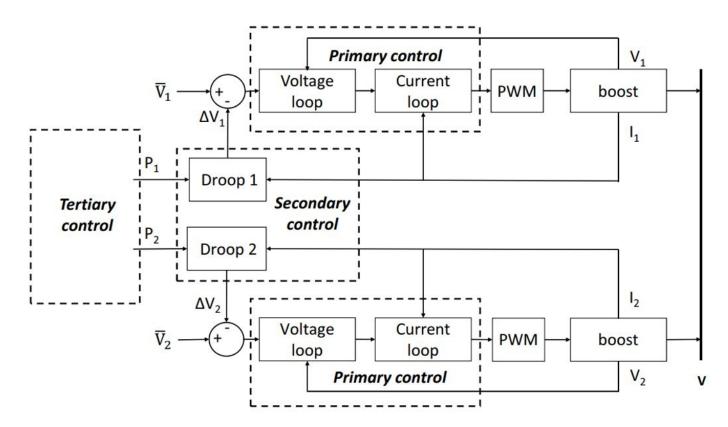


- The combination of both generators under *droop control*, allows to construct a hierarchical structure with three levels of regulation.
- A primary level devoted to regulate electrical variables at the power converter circuit.
- The secondary level defines, by mean of droop resistances, the proportion of power shared among generators.
- The third level or tertiary control will be able to modify the amount of power provided by any generation unit attending dispatch policies.





#### **Levels of control**





## **III. Optimization strategy**





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- The only way to change that proportion will be modifying the parameter accordingly.
- If environmental conditions alter the availability of any of the power resources, the proportions of generation should adapt to those circumstances.
- To define the change of proportions, economic dispatch principles can be adapted to the case of renewable resources.





In this work the cost models for renewable sources are taken from: M. M. Hoogwijk, "On the global and regional potential of renewable energy sources", Ph.D. Thesis at Faculteit Scheikunde, Universiteit Utrecht, 2004.



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$$C(P) = (\alpha \times \mathcal{I} \times P) + (\mathcal{M} \times P),$$

being  $\alpha$  the annuity factor,  $\mathcal{I}$  the investment cost per unit power P installed and  $\mathcal{M}$  the maintenance cost per unit power P installed. In particular, employing the information provided





Parameter	Description	Value
α	Annuity factor per hour	0.04
$\mathcal{I}_1$	Investment cost per kW/hour of PV power installed	\$781.85
$\mathcal{I}_2$	Investment cost per kW/hour of bat- tery power installed	\$390.92
$\mathcal{M}_1$	Maintenance cost per kW/hour of PV power installed	\$7.04
$\mathcal{M}_2$	Maintenance cost per kW/hour of battery power installed	\$3.9

Values adapted to Colombian pesos, from https://www.irena.org



# **Optimal cost**



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 In accordance, the minimum cost will be achieved by defining and solving an optimization problem.



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minimize 
$$C(P_1, P_2)$$
  
subjected to  $P_1 + P_2 = 1500 W$ .





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- It represents a reduced computational load for calculations of minimal points in PSIM.
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$$\Gamma(P_1, P_2) = (38.314 \times P_1)^2 + (19.5368 \times P_2)^2$$
  
=  $(1467.96 \times P_1^2) + (381.69 \times P_2^2)$ ,

and then minimizing  $\Gamma(P_1, P_2)$  corresponds to minimize  $C(P_1, P_2)$ , as it can be easily shown that  $\Gamma \geq C$ .





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- That proportion of power is used to update the values of the *droop parameter* at each generator.
- The implementation of the Newton-Raphson algorithm in PSIM was accomplished by coding in a C-block a recursive equation obtained analytically by the method of Lagrange multipliers.



#### **IV. Results**





• Circuit realizations for the DC microgrid in PSIM, were employed as test bed to verify the appropriate operation of the optimization scheme proposed.



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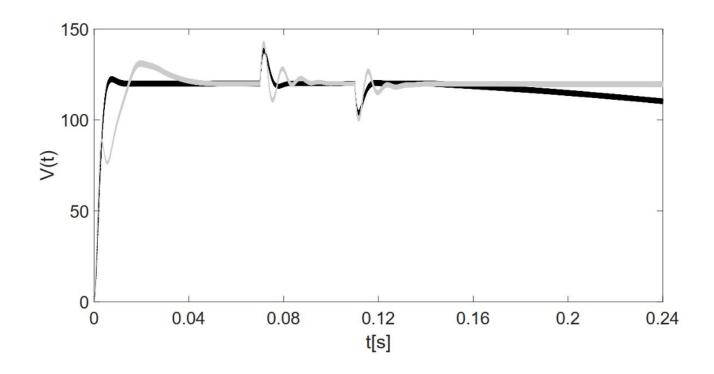
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- An initial set of simulations are taken within the interval t = [0, 0.24].
- The system transient is experienced until t = 0.07, where a step variation of the load is applied.
- for t = 0.11 the load value return to the nominal condition.
- for t > 0.14 the input voltage at the photovoltaic unit is modified by a decaying lobe emulating the reduction in solar radiation after the noon.

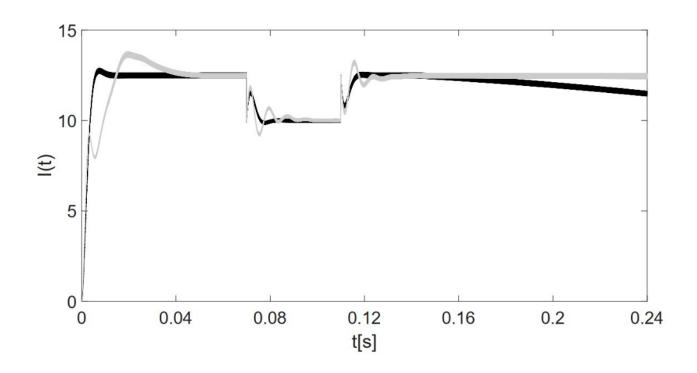








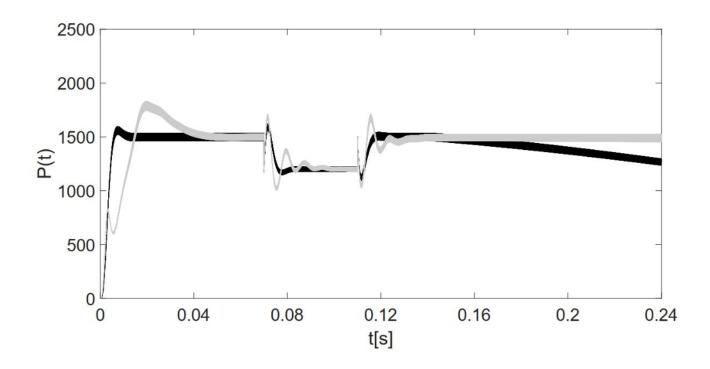








# **Primary control**







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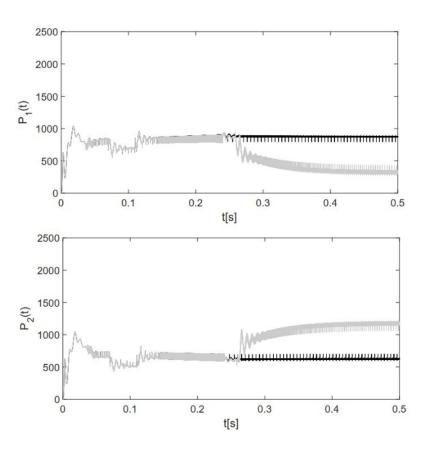
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- The optimal power values obtained at simulations can be easily verified analytically.
- By contrast, a fixed power sharing of 60% 40% is overimposed.



# **Dynamic droop**



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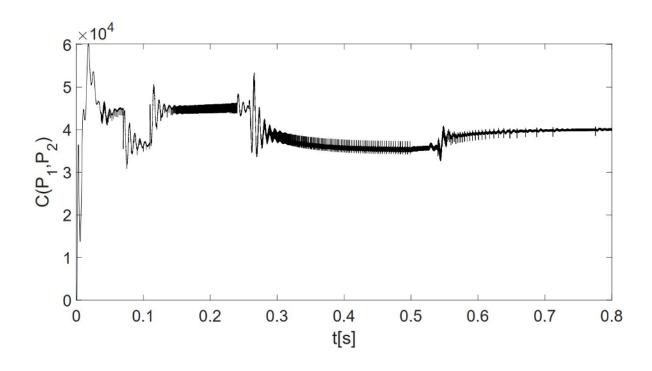
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- The analysis for the cost function over the whole time interval suggest that it is minimal just after the optimization algorithm starts performing calculations.
- Also, it is important to notice that despite the increase of costs after altering the function of the battery bank, it is not higher than the initial (unoptimized) value.









### V. Conclusions





 An optimal management scheme for an isolated microgrid operating in DC has been proposed by applying cost functions for renewable resources suggested in the literature. The optimal problem was solved numerically employing a Newton-Raphson approach.



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- Simulation results performed in PSIM allowed to verify the dynamic calculations for droop parameters and the corresponding adaptation of power proportions to environmental changes in the system.
- Ongoing work is currently devoted to experimental verification of the proposed management strategy on a laboratory prototype built at the Universidad Industrial de Santander.



# **Acknowledgements**



### **Acknowledgements**

Authors wanted to acknowledge the financial support of the Universidad Industrial de Santander under the grant code VIE-UIS 2479, funding the project entitled: "Control centralizado para un sistema de generación de energía con potencial aplicación en zonas rurales del departamento de Santander".



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### **Questions?**

### Thank you for your attention !!!

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