



XSICEL 2021

Transición energética en la 4ta revolución industrial



Universidad
Tecnológica
de Pereira



UNIVERSIDAD
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DE COLOMBIA

Overcurrent protection of active distribution networks: A comparative review

B. Grisales-Soto, S. Pérez-
Londoño, J. Mora-Flórez

Universidad Tecnológica de
Pereira

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- II. Conventional approach for overcurrent relays coordination
- III. Adaptive approach for overcurrent relays coordination
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I. Introduction



1. Decarbonisation of the energy sector.



2. Integration of Distributed Energy Resources (DER).



3. Transition to Active Distribution Networks (ADN)



II. Conventional approach for overcurrent relay coordination

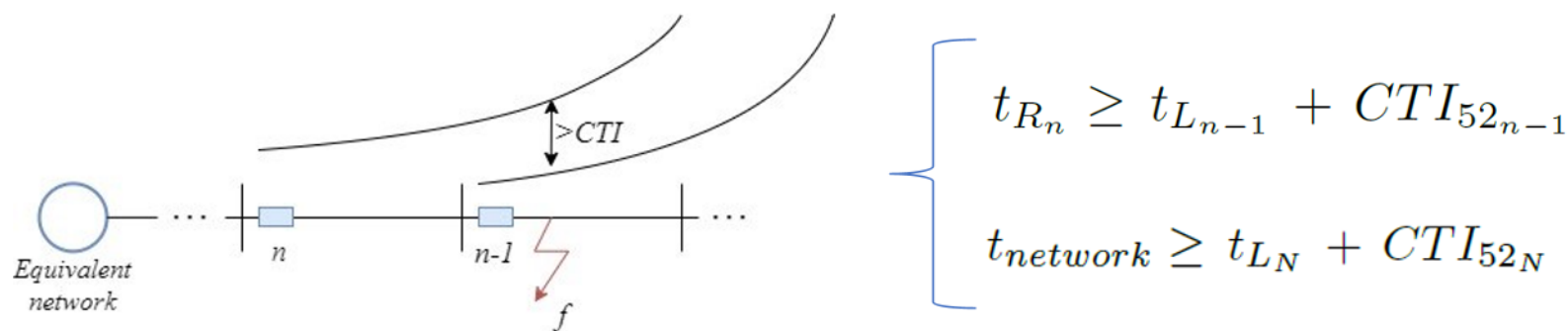


Fig 1. Coordinated 51 relays.

The operation time is defined by the according to the IEC 255 standard.

$$t_{op} = \frac{A}{M^P - 1} TDS \quad M = \frac{I_F}{I_p}$$

III. Adaptive approach for overcurrent relay coordination

1. Sequence currents based adaptive protection approach for DN's with DER

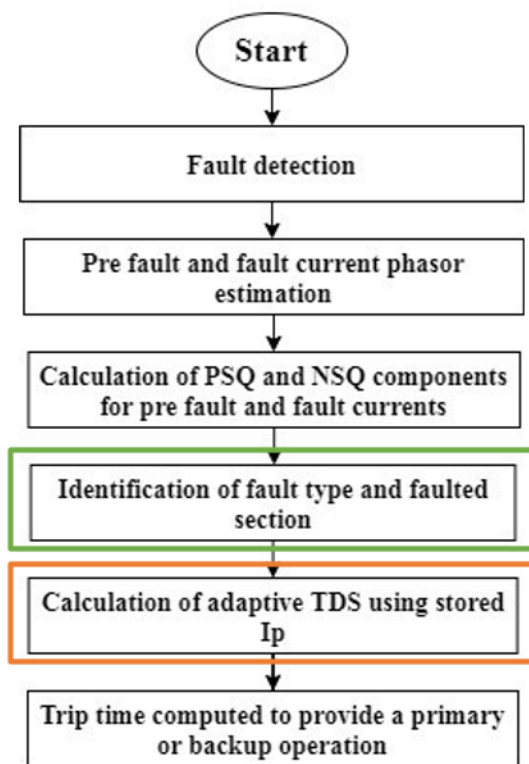


Fig 2. Flow chart of the adaptive approach I.

Positive sequence component

$$t_{p-ij}^c = \frac{0.14}{\left(\left(I_{1Fij}^c / I_{pj}^c\right)^{0.02} - 1\right)} TDS_{pj}^c$$

Negative sequence component

$$t_{b-ij}^c = \frac{0.14}{\left(\left(I_{2Fij}^c / I_{bj}^c\right)^{0.02} - 1\right)} TDS_{bj}^c$$

The relay computes the **adaptive-TDS** when a fault has occurred

$$TDS_{new} = \frac{(M)_{new}^P - 1}{(M)_{old}^P - 1} TDS_{old}$$

2. Superimposed Adaptive Sequence Current Based Microgrid Protection: A New Technique

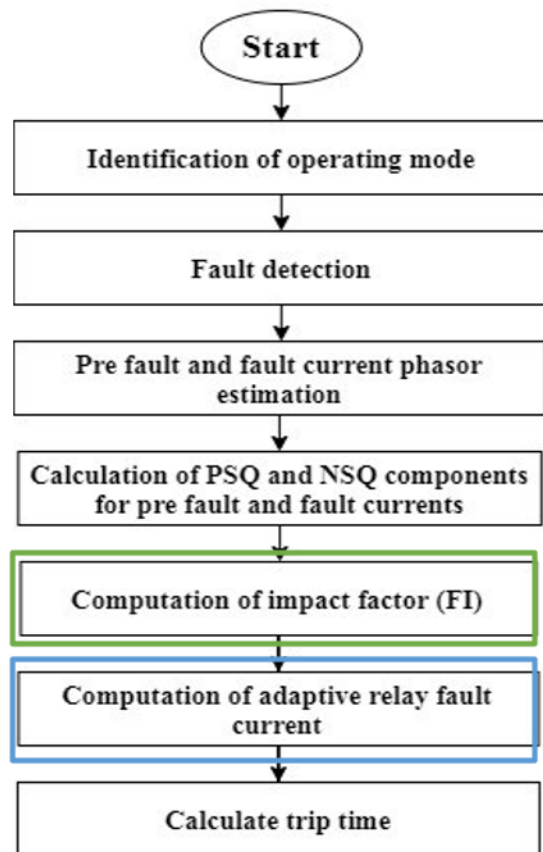


Fig 3. Flow chart of the adaptive approach II.

Impact factor (FI) based on the operation of the microgrid.

$$FI = \frac{|\Delta I_{1F}|}{|1 - I_{1F}| |1 - \Delta I_{1F}| |I_{1pre}|} \quad FI = \frac{|\Delta I_{1F}| - |I_{1pre}|}{|\Delta I_{1F}|}$$

Adaptive fault current.

$$I_{F_{ad}} = (I_{1F} + I_{2F})(FI)$$

Depending on the change of the operating mode, the authors propose the calculation of an **new TDS**.

$$TDS_{new} = \frac{(M)_{old}^P - 1}{(M)_{new}^P - 1} TDS_{old}$$

3. Dynamic adaptive protection for distribution systems in Grid-Connected and Island Modes

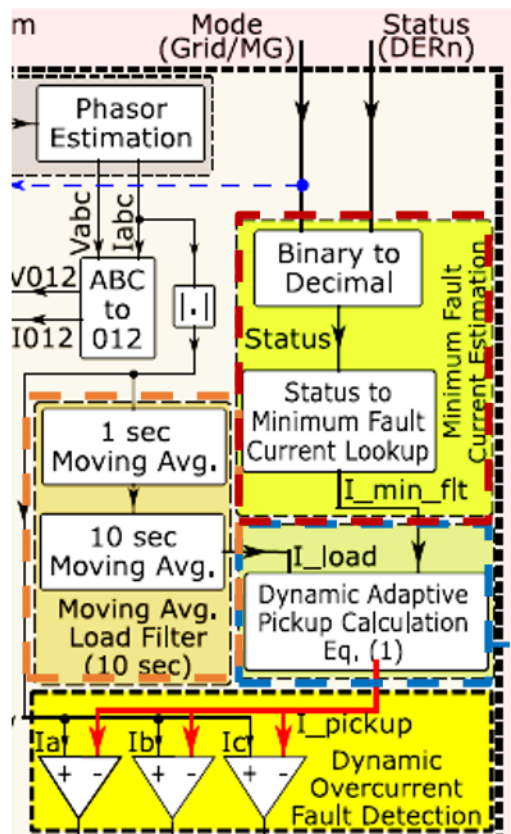


Fig 4. Overview of the adaptive approach III.

→ The paper is focused on the estimation of an **Dynamic Adaptive Pickup current** ($I_{p_{ad}}$)

$$I_{p_{ad}} = a I_{mov_{10s}} + b (I_{F_{DERs}} - a I_{mov_{10s}})$$

- $I_{mov_{10s}}$ is a 10-second moving average window filter.
- $I_{F_{DERs}}$ is the minimum fault current estimation.

4. An adaptive directional current protection scheme for distribution network with DERs

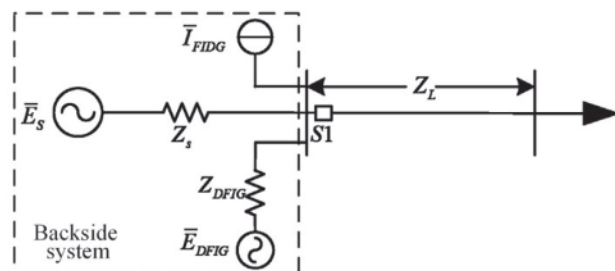


Fig 5. Equivalent circuit of simple ADN

The system at the backside of the protection could be replaced with a equivalent after fault occurred.

The setting formula



$$I_{p_{ad}} = \frac{K_{rel} K_d \bar{E}_e}{Z_e + Z_L}$$

When the fault location $\alpha < \beta$

$$I_{p_{ad}} = \frac{\sqrt{3}}{2} \left| \frac{\bar{E}_e}{Z_e + \alpha Z_L} \right| > \frac{\sqrt{3}}{2} \left| \frac{\bar{E}_e}{Z_e + \beta Z_L} \right|$$

When the fault location $\alpha > \beta$

$$I_{p_{ad}} = \frac{\sqrt{3}}{2} \left| \frac{\bar{E}_e}{Z_e + \alpha Z_L} \right| < \frac{\sqrt{3}}{2} \left| \frac{\bar{E}_e}{Z_e + \beta Z_L} \right|$$

IV. Results

Test system

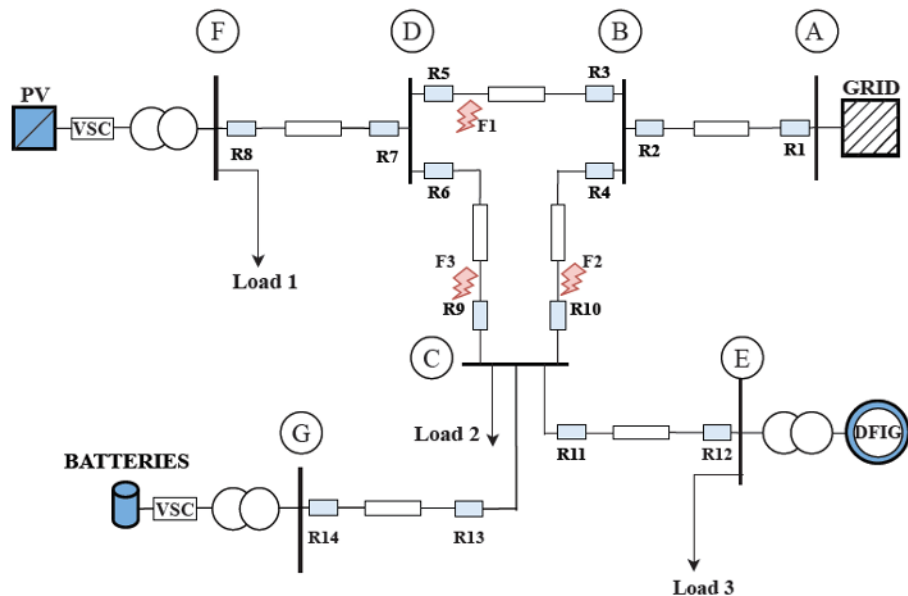


Fig. 6. ADN used as test system.



Mode I: all sources are on.

Mode II: only the DFIG based DER is on.

Mode III: only the PV-based DER is on.

IV. Results

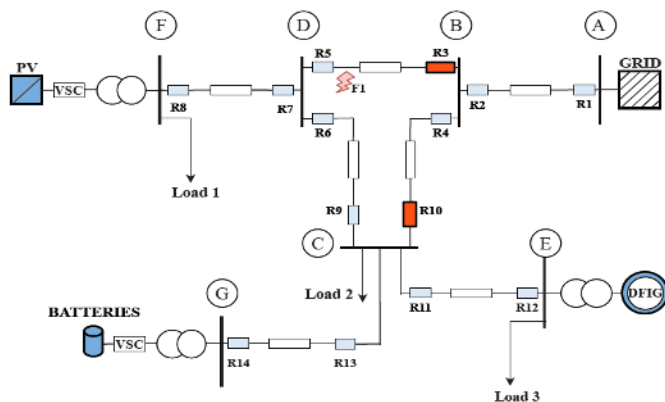


Fig 7. Primary and back-up relay for F1.

Mode I: all sources are on.

Mode II: only the DFIG based DER is on.

Mode III: only the PV-based DER is on.

Test Results - Conventional Approach

Fault	Relay		Mode I			Mode II			Mode III		
	PR	BR	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt
F1	3	10	0.296	0.441	0.145	0.315	0.121	-0.194	0.317	0.119	-0.198

Test Results - Adaptive Approach I

Fault	Relay		Mode I			Mode II			Mode III		
	PR	BR	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt
F1	3	10	0.296	0.441	0.145	0.276	0.421	0.145	0.296	0.452	0.156

Test Results - Adaptive Approach II

Fault	Relay		Mode I			Mode II			Mode III		
	PR	BR	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt
F1	3	10	0.297	0.407	0.110	0.297	0.411	0.114	0.323	0.457	0.134

IV. Results

Test Results - Conventional Approach											
Relay			Mode I			Mode II			Mode III		
Fault	PR	BR	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt
F1	3	10	0.296	0.441	0.145	0.315	0.121	-0.194	0.317	0.119	-0.198

Test Results - Adaptive Approach I											
Relay			Mode I			Mode II			Mode III		
Fault	PR	BR	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt
F1	3	10	0.296	0.441	0.145	0.276	0.421	0.145	0.296	0.452	0.156

Test Results - Adaptive Approach II											
Relay			Mode I			Mode II			Mode III		
Fault	PR	BR	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt	t_{PR}	t_{BR}	Δt
F1	3	10	0.297	0.407	0.110	0.297	0.411	0.114	0.323	0.457	0.134

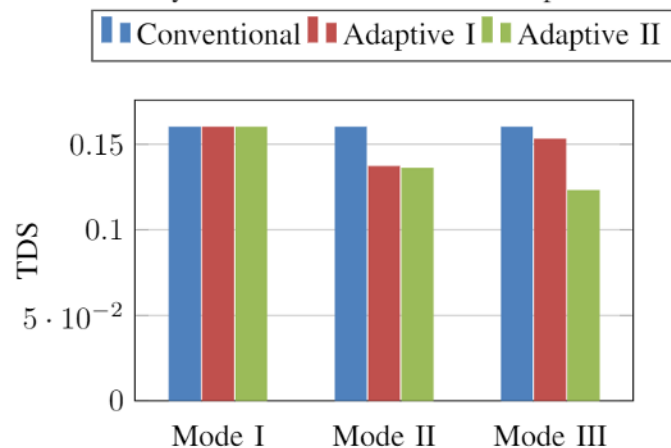


Fig 7. Relay R3's TDS for each mode operation.

IV. Results

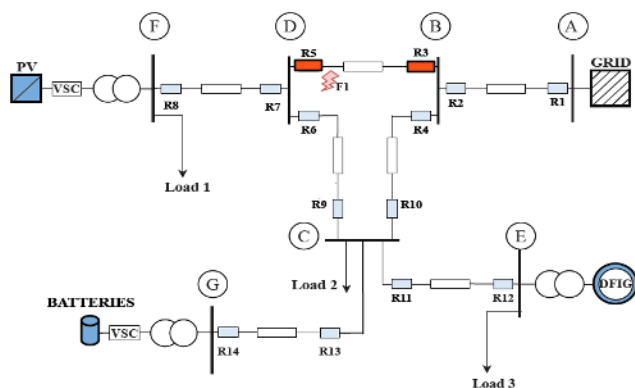


Fig 8. Primary relay for F1.

Mode I: all sources are on.

Mode II: only the DFIG based DER is on.

Mode III: only the PV-based DER is on.

Test Results - Adaptive Approach III

Relay		Mode I			Mode II			Mode III		
Fault	PR	I_{pad}	I_F	Trip	I_{pad}	I_F	Trip	I_{pad}	I_F	Trip
F1	5	33	854	Yes	43	636	Yes	40	669	Yes
	3	30	707	Yes	40	574	Yes	26	560	Yes

Test Results - Adaptive Approach IV

Relay		Mode I			Mode II			Mode III		
Fault	PR	I_{pad}	I_F	Trip	I_{pad}	I_F	Trip	I_{pad}	I_F	Trip
F1	5	941	1255	Yes	910	1214	Yes	931	1241	Yes
	3	1356	1808	Yes	1343	1791	Yes	1340	1787	Yes

VI. Conclusions

- An ADN has different operating modes and the conventional approach does not guarantee overcurrent relay coordination.
- Adaptive approaches I and II can provide a solution to coordination with the calculation of TDS and I_p for each operation mode. However, these schemes use adaptive parameters estimated using the fault voltages and currents.
- The approach III requires communication infrastructure, making the proposed scheme expensive and vulnerable to cyber-attacks.
- Approach IV presents an adequate performance without communication infrastructure but has a long time to detect the fault.

VII. Questions



Image taken from: <https://www.pngwing.com/es/free-png-ybhlm>.